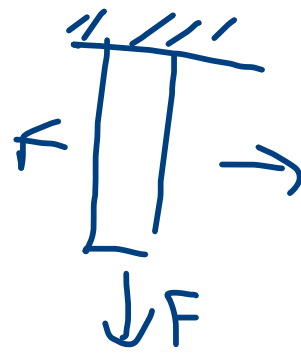


# VÍCEOSÁ NAPJATOST

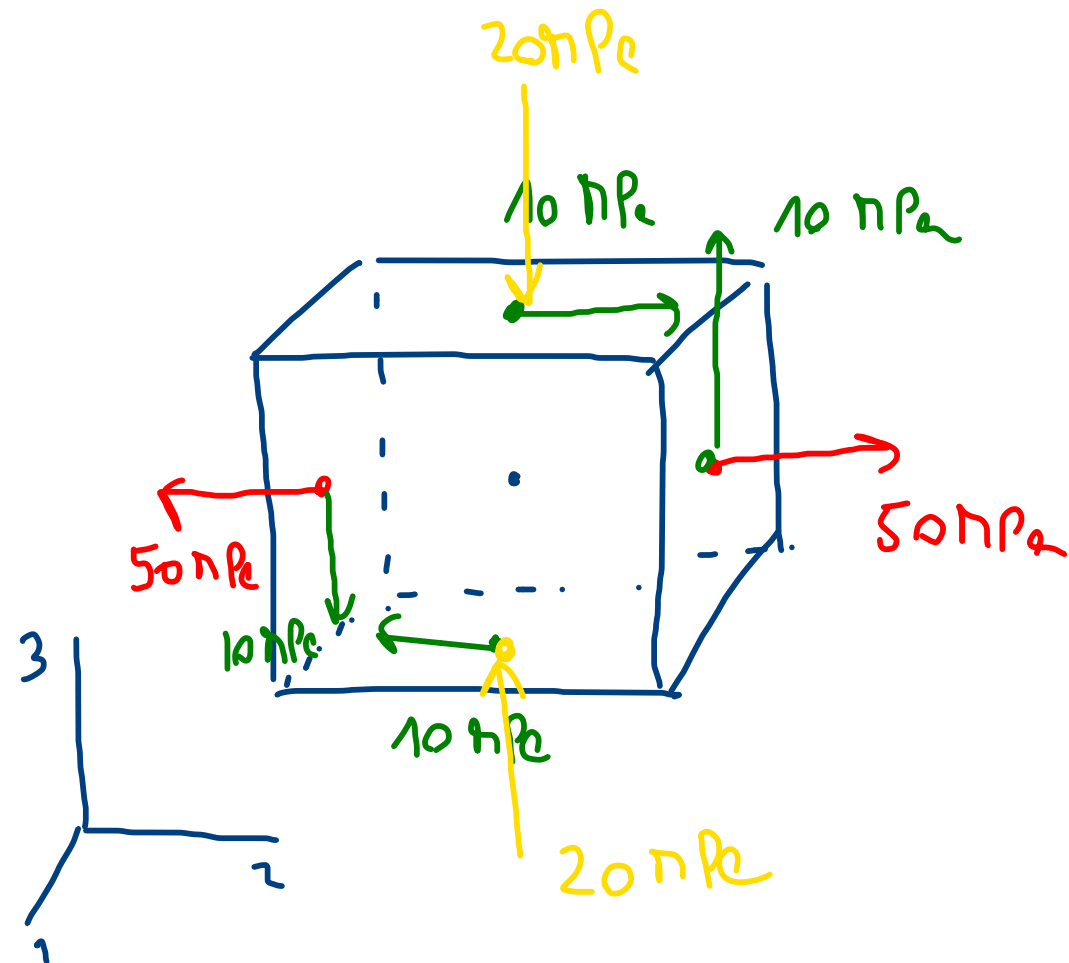
$$\underline{\underline{\sigma}} \equiv \underline{\underline{\epsilon}}$$

$$\underline{\underline{\sigma}} = E \cdot \underline{\underline{\epsilon}} \quad (\text{JEDNOSOÁ NAPJATOST})$$



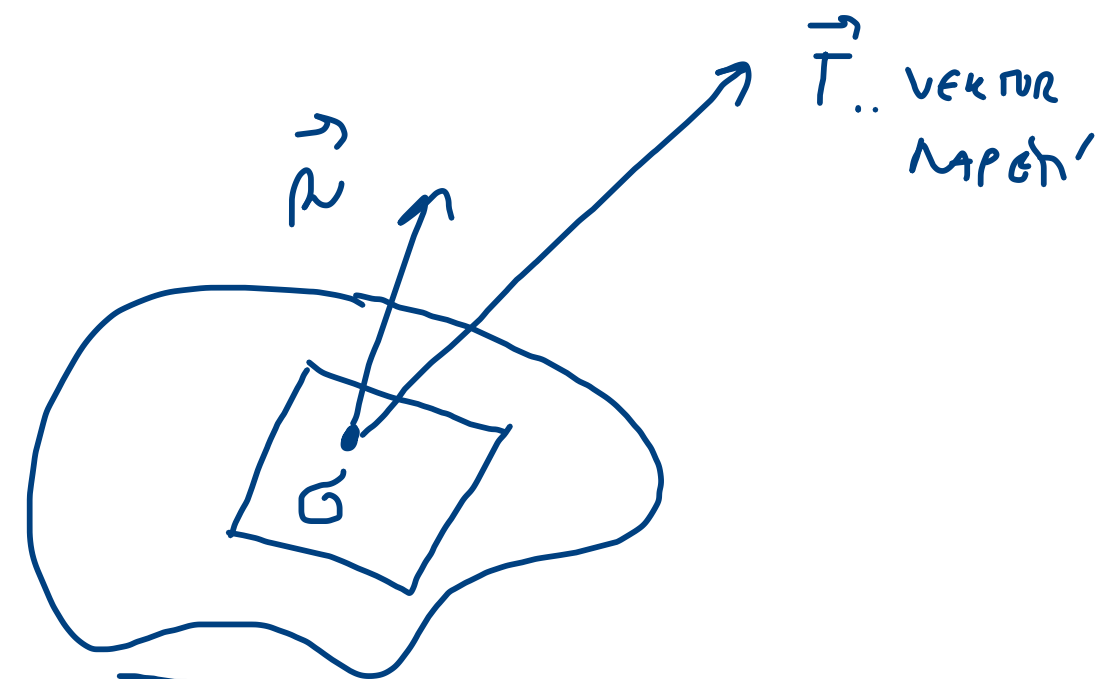
TENZOR NAPĚTÍ

$$\sigma_{ij} = \begin{pmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{pmatrix}$$



$$\sigma_{ij} = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 50 & 10 \\ 0 & 10 & -20 \end{pmatrix} \text{ MPa}$$

SHYKOVÉ STŘEŽY  
 NORMÁLOVÉ STŘEŽY  
 NORMÁLOVÉ STŘEŽY



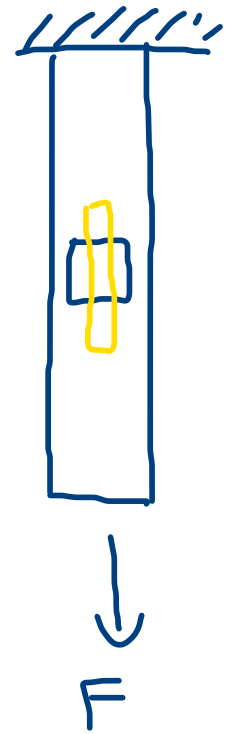
$$\vec{T} = \underline{\underline{\sigma}} \cdot \vec{n}$$

$$T_i = \sum_{j=1}^3 \sigma_{ij} n_j$$

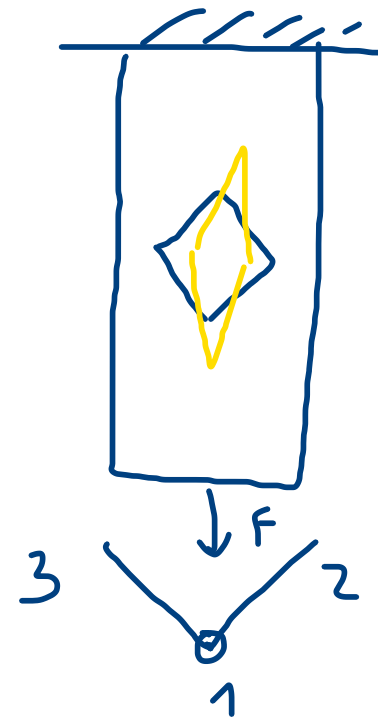
$$T_2 = \sigma_{21} n_1 + \sigma_{22} n_2 + \sigma_{23} n_3$$

# Hlavní směry, hlavní napětí a hlavní deformace

Pr1



$$\sigma_{ij} = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & F/s \end{pmatrix}$$



$$\sigma_{ij} = \begin{pmatrix} 0 & 0 & 0 \\ 0 & F/2s & F/2s \\ 0 & F/2s & F/2s \end{pmatrix}$$

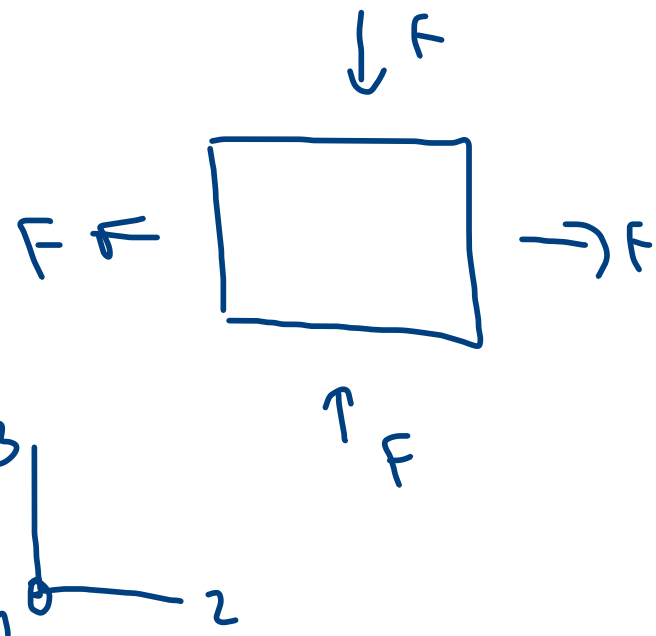
$$\sigma_{ij} = \begin{pmatrix} \sigma_1 & 0 & 0 \\ 0 & \sigma_2 & 0 \\ 0 & 0 & \sigma_3 \end{pmatrix}$$

$\sigma_1, \sigma_2, \sigma_3 \dots$  Hlavní napětí

$$\epsilon_{ij} = \begin{pmatrix} \epsilon_1 & 0 & 0 \\ 0 & \epsilon_2 & 0 \\ 0 & 0 & \epsilon_3 \end{pmatrix}$$

$\epsilon_1, \epsilon_2, \epsilon_3 \dots$  Hlavní deformace

Pr2

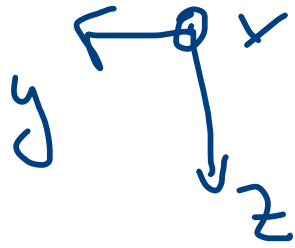


$$\sigma_{ij} = \begin{pmatrix} 0 & 0 & 0 \\ 0 & F/s & 0 \\ 0 & 0 & F/s \end{pmatrix}$$

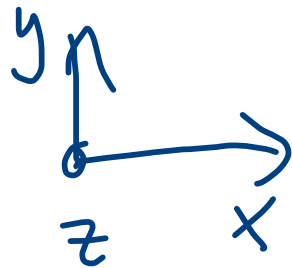
$$\sigma_{ij} = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & F/s \\ 0 & F/s & 0 \end{pmatrix}$$

hlavní směry

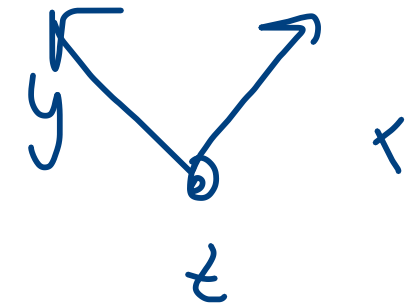
$$\vec{g} = \begin{pmatrix} 0 \\ 0 \\ 10 \end{pmatrix} \text{ m/s}^2$$



$$\vec{g} = \begin{pmatrix} 0 \\ -10 \\ 0 \end{pmatrix} \text{ m/s}^2$$



$$\vec{g} = \begin{pmatrix} -\frac{10}{\sqrt{2}} \\ \frac{10}{\sqrt{2}} \\ 0 \end{pmatrix} \text{ m/s}^2$$



$$\underline{\underline{\sigma}} = \begin{pmatrix} 10 & 20 & 30 \\ 20 & 0 & 50 \\ 30 & 50 & 60 \end{pmatrix} \text{ MPa}$$

ТЕНЗОР НАПРЯЖЕНИЙ  
DEFORMATION

СИММЕТРИЧЕСКИЙ

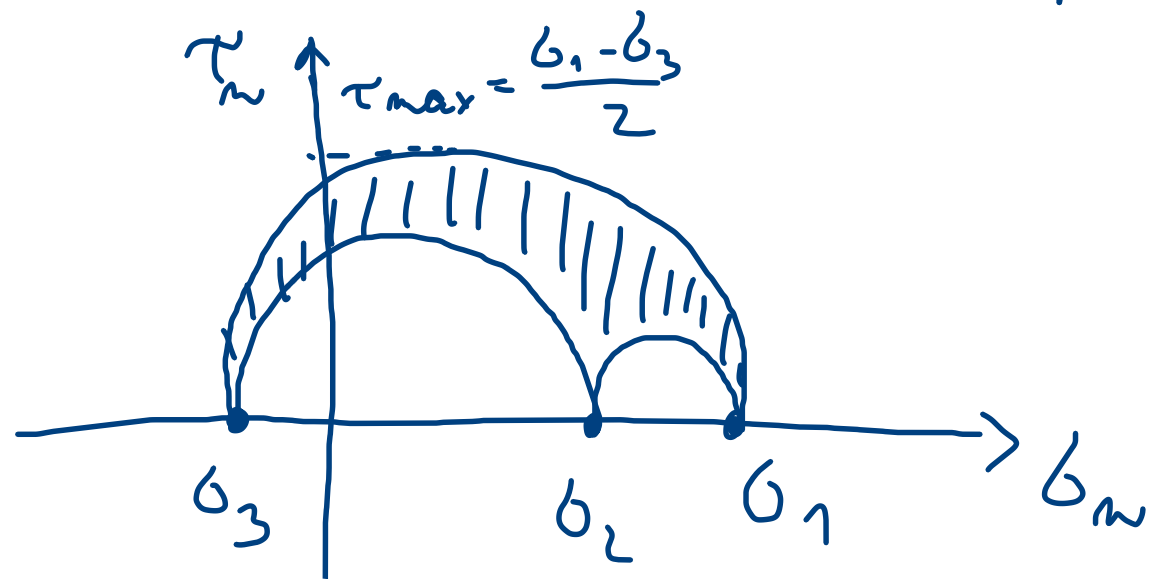
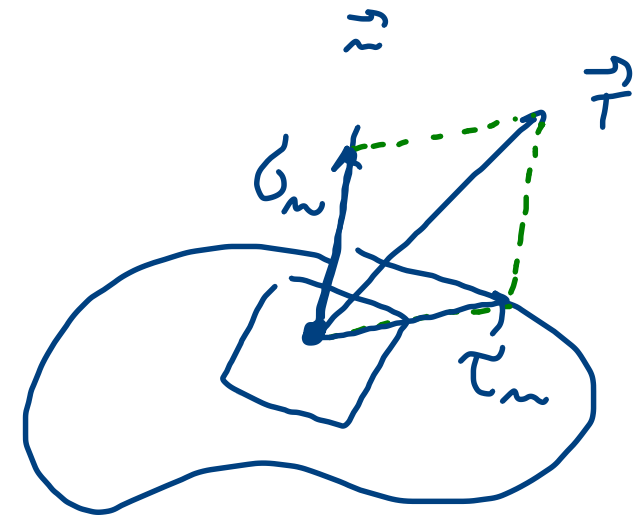


МАТРИЦА НАПРЯЖЕНИЙ ... ВЛАСТЫЕ НАПРЯЖЕНИЯ

МАТРИЦА СМЯТЫ ... ВЛАСТЫЕ СМЯТЫ

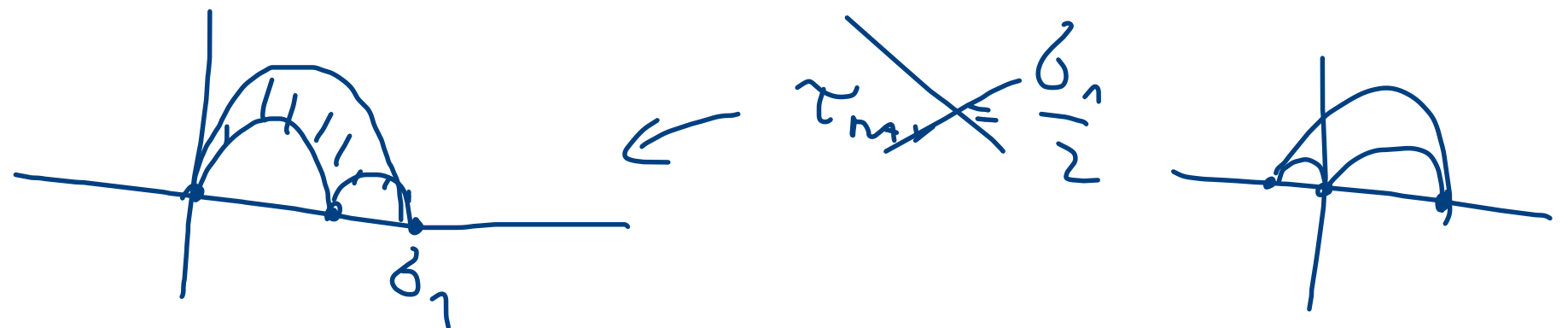
# Mohrovy kružnice

HLAVNÍ NAPĚTÍ  $\sigma_1, \sigma_2, \sigma_3$   
 30MPa      10MPa  
 30MPa      10MPa

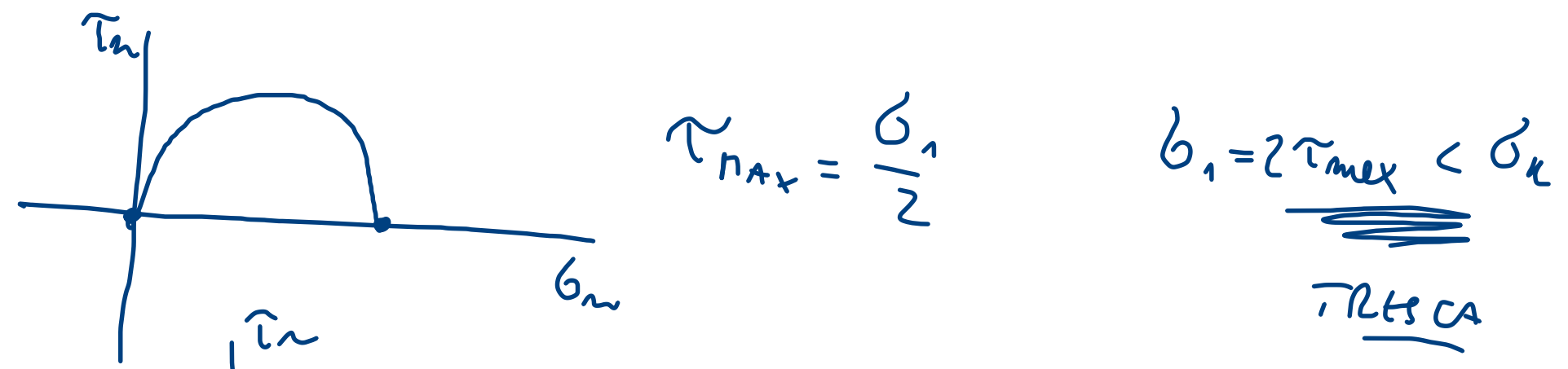


a) 30SA' NAPĚTOST

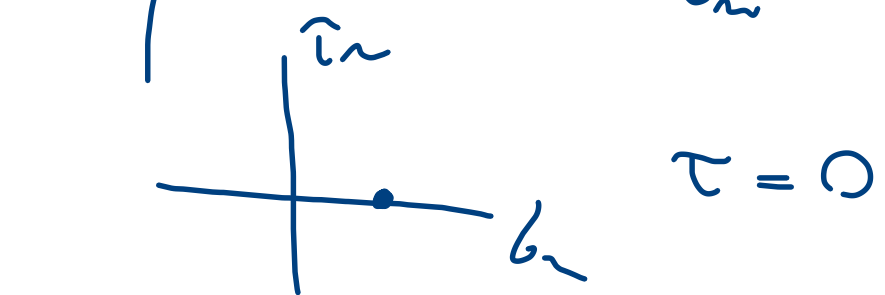
b) DVOUSA' NAPĚTOST ... sigma\_3 = 0



c) JEDNOUSA' NAPĚTOST ... sigma\_2 = sigma\_3 = 0



d) HYDROSTATICKA' NAPĚTOST  
 $\sigma_1 = \sigma_2 = \sigma_3$



$\sigma_1 = 2 \tau_{max} < \sigma_k$   
TRH CA

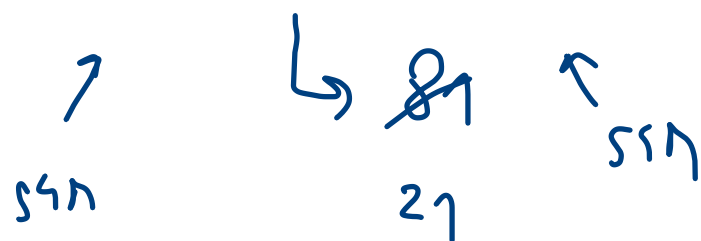
# Hookeův zákon při víceosé napjatosti

1 osá n.  $\sigma = E \cdot \varepsilon$        $\varepsilon = \frac{1}{E} \sigma$

3 osá n.  $\sigma_{ij} = C_{ijkl} \varepsilon_{kl}$

~~$\sigma_{ij} = E \cdot \varepsilon_{ij}$~~

~~$\sigma_{23} = E \varepsilon_{23}$   
 $\sigma_{12} = E \varepsilon_{12}$~~



$C_{ijkl}$    
 Anizotropní materiál   
 { zákonů ... 21   
 { konstant ... 3

izotropní materiál ... 2 ( $E, \mu$ ) → hodily ve složku   
 $G = \frac{E}{2(1+\mu)}$

ortotropní (120°)   
 ↪ 9

Hookeův zákon   
 pro izotropní materiál   
 (3 osá napjatost)

$$\sigma_{ij} = \frac{E}{1+\mu} \left[ \varepsilon_{ij} + \frac{\mu}{1-2\mu} \delta_{ij} \varepsilon_{kk} \right]$$

$$\varepsilon_{ij} = \frac{1+\mu}{E} \sigma_{ij} - \frac{\mu}{E} \delta_{ij} \sigma_{kk}$$

$\delta_{ij} = \begin{cases} 1 & i=j \\ 0 & i \neq j \end{cases}$

$$\varepsilon_{kk} = \sum_{k=1}^3 \varepsilon_{kk}$$

$$\sigma_{kk} = \sum_{k=1}^3 \sigma_{kk} = \sigma_{11} + \sigma_{22} + \sigma_{33}$$

HOOKEÏO ZÁNON PRO IZOTROPÍ KONTINÚOY  
(2 ΘΑΪ ΜΡΩΤΟΣ)

$$\varepsilon_1 = \frac{1}{E} (\sigma_1 - \mu \sigma_2)$$

$$\varepsilon_2 = \frac{1}{E} (\sigma_2 - \mu \sigma_1)$$

$$\sigma_1 = \frac{E}{1-\mu^2} (\varepsilon_1 + \mu \varepsilon_2)$$

$$\sigma_2 = \frac{E}{1-\mu^2} (\varepsilon_2 + \mu \varepsilon_1)$$

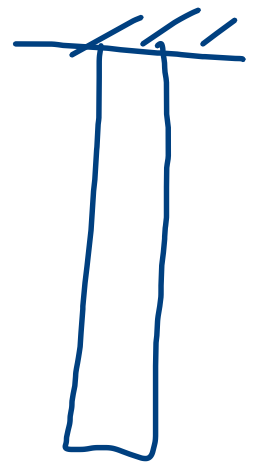
~~$$\sigma_1 = E \varepsilon_1$$~~

~~$$\sigma_2 = E \varepsilon_2$$~~

# PEUNOST

$$\sigma = \epsilon \cdot E$$

Hooké

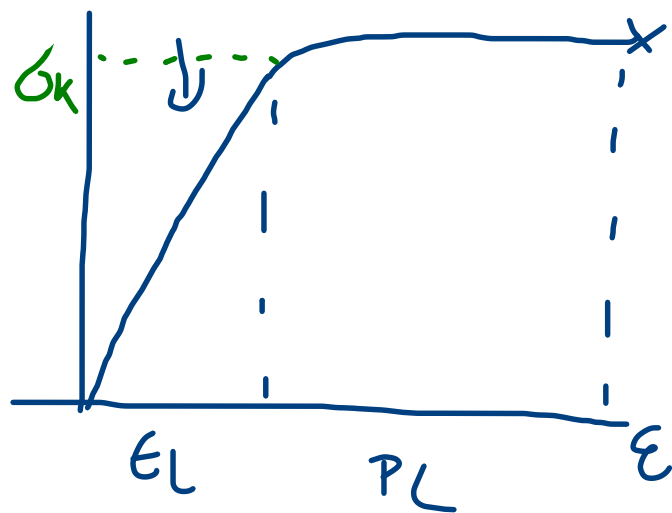


$$\delta = \frac{F}{S}$$

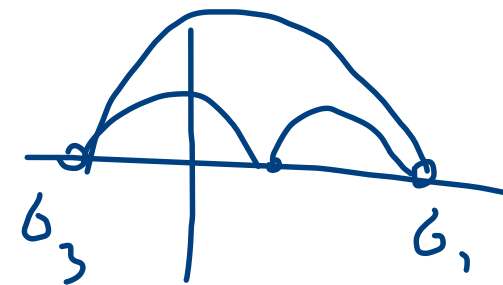


F

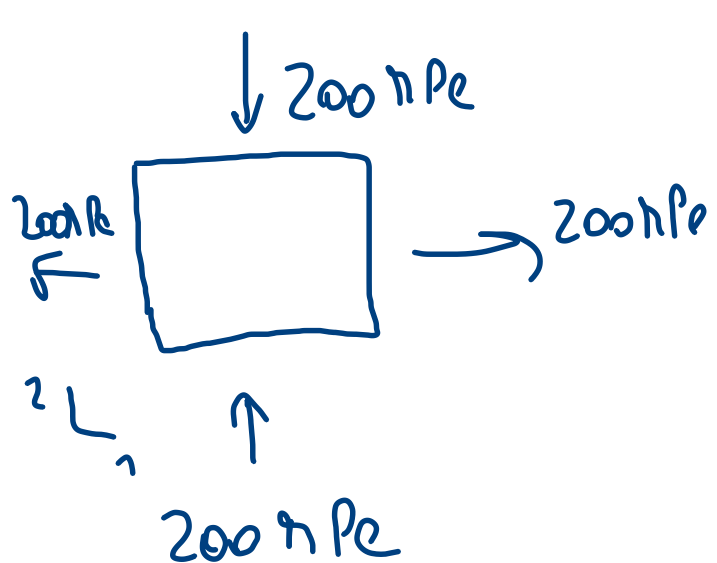
$$\sigma_k = 300 \text{ MPa}$$



105E' KAMPAIN!



$$\tau_{max} = \frac{(\sigma_1 - \sigma_3)}{2}$$



$$\sigma_{ij} = \begin{pmatrix} 200 & 0 & 0 \\ 0 & 200 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

$$\dots \begin{cases} \sigma_1 = 200 \text{ MPa} \\ \sigma_2 = 200 \text{ MPa} \\ \sigma_3 = 0 \end{cases}$$

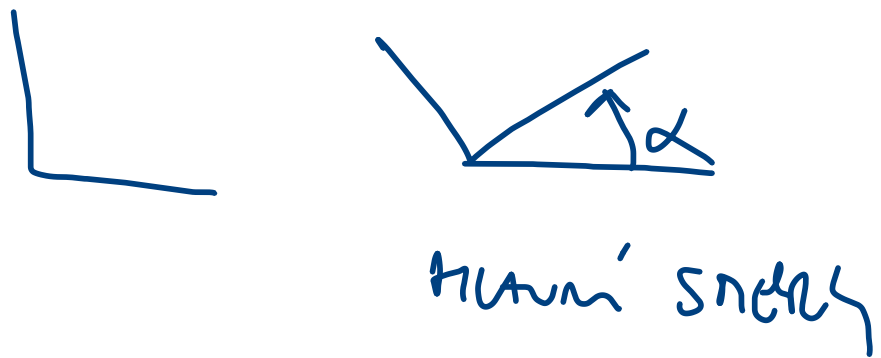
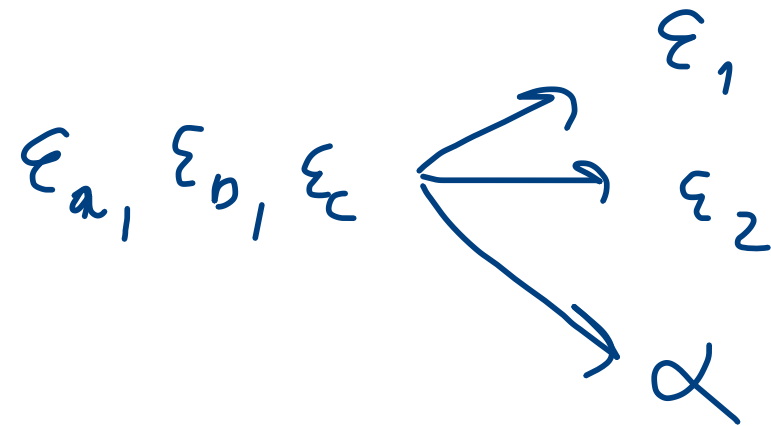
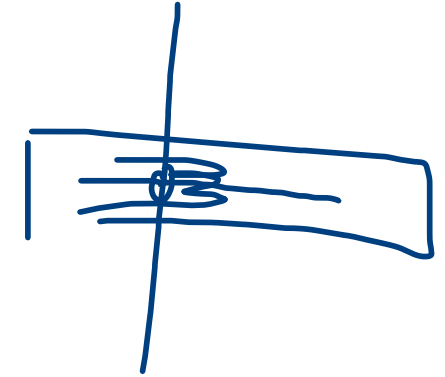
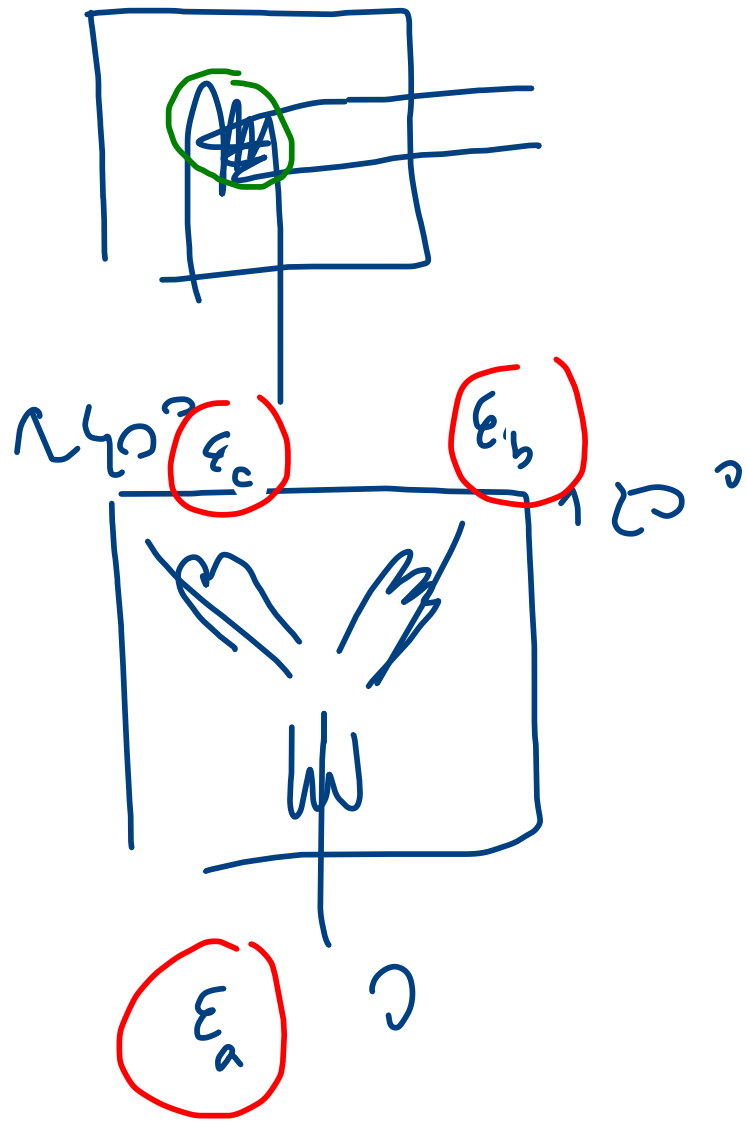
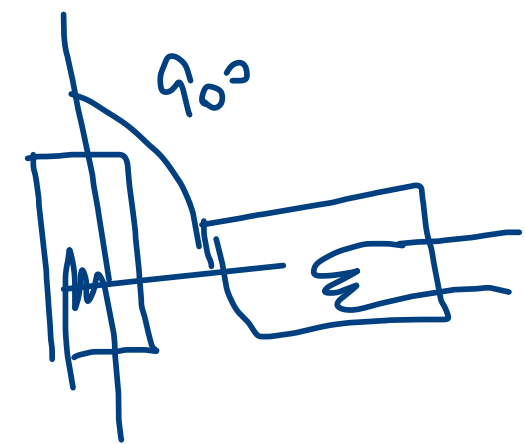
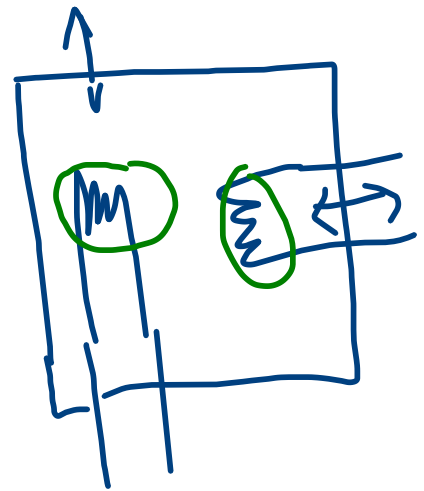
$\sigma_{REIN}$   $\left\{ \begin{array}{l} \text{H H H} \\ \text{(von Mises)} \end{array} \right. \dots \sigma_{REIN}$

TRESCA ...  $\sigma_{TRESCA} = 2 \cdot \tau_{max}$

$$\sigma_{REIN} = \frac{1}{\sqrt{2}} \sqrt{(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2}$$

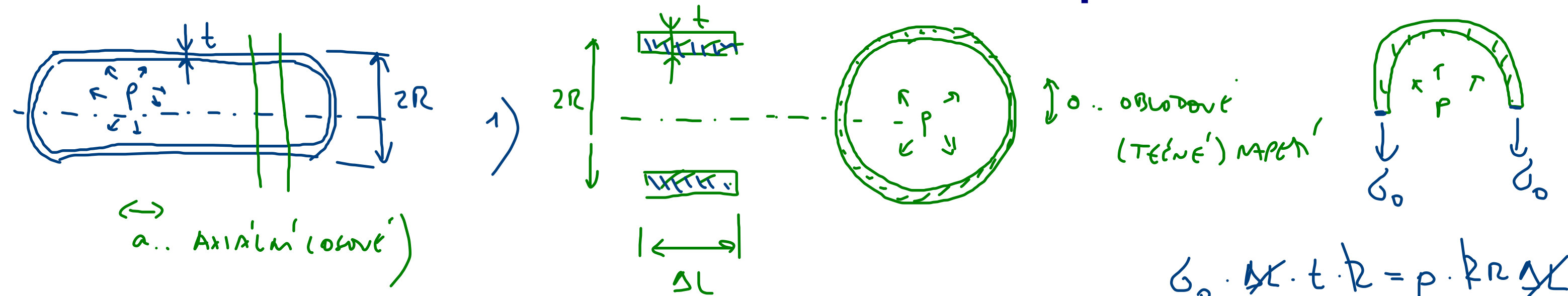
VON MISES FOND MAPEN!

# Měření dvouosé napjatosti - tenzometrické růžice (rozety)





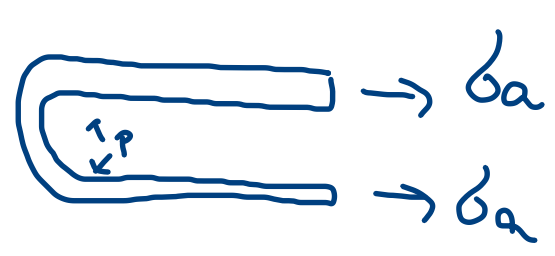
# Tenkostěnná válcová nádoba zatížená vnitřním přetlakem



$$\sigma_0 \cdot \Delta L \cdot t \cdot R = p \cdot R \Delta L$$

$$\sigma_0 = p \cdot \frac{R}{t}$$

2) Axialní



$$\sigma_a \cdot 2tR \cdot t = p \cdot tR$$

$$\sigma_a = p \cdot \frac{R}{2t}$$

$$t \ll R$$

	$\sigma_0 = 2 \cdot \sigma_a$	$\frac{\sigma_0}{\sigma_a} = 2$
$\epsilon_0$	<del><math>\epsilon_0 = 2 \epsilon_a</math></del>	$\frac{\epsilon_0}{\epsilon_a} = ?$

Pozn.:

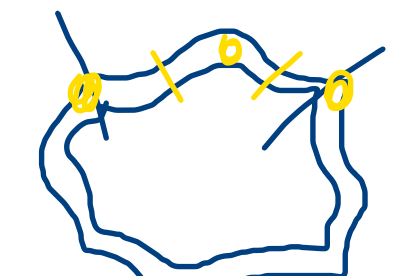
kovl t

$$\sigma_a = \sigma_0 = p \frac{R}{2t}$$

Pozn.:



$$t, s \dots \sigma_{max} \approx 10 \times \sigma_0$$



$\Rightarrow$

